

APPLICATION

FOR

UNITED STATES LETTERS PATENT

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FOR

PERMANENTLY WETTABLE SUPERABSORBENTS

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## PERMANENTLY WETTABLE SUPERABSORBENTS

### 10 Technical Field

The invention relates to superabsorbents, more particularly to superabsorbent fibers that are permanently wettable.

### Background of the Invention

The use of water-swellaable, generally water-insoluble absorbent materials, commonly known as superabsorbents, in disposable absorbent personal care products is well known. Such absorbent materials are generally employed in absorbent products such as diapers, training pants, adult incontinence products, and feminine care products in order to increase the absorbent capacity of such products while reducing their overall bulk. Absorbent materials are generally present as superabsorbent particles in a fibrous matrix, such as a matrix of wood pulp fluff.

Superabsorbent particles are sometimes difficult to use because they do not remain stationary during the manufacturing process and may shift position in the article. The potential advantages of using superabsorbent fibers, as opposed to superabsorbent particles, include improved product integrity, better containment, and improved absorbent properties, such as rapid fluid absorption and fluid distribution properties. The use of superabsorbent fibers may also lead to improved product attributes, such as thinner and softer products that provide a better fit, less gel migration, and potential simplification of product manufacturing processes.

The surface characteristics of superabsorbent fibers play a central role in determining the fluid handling properties of composites that contain them. Accordingly, there is a need for superabsorbent fibers having sufficient surface wettability. Commercially available superabsorbent fibers do not exhibit permanent wettability.

### Summary of the Invention

The invention includes methods of making permanently wettable superabsorbent material involving treating the superabsorbent material with a surfactant solution. A surfactant is used that has at least one functional group that is reactive with the superabsorbent material and at least one non-reactive and hydrophilic functional group. The surfactant is applied to the superabsorbent material when functional groups on the surface of the superabsorbent material are in an activated state. In one embodiment, the surfactant is applied to the superabsorbent material when the superabsorbent material is solvated. Desirably, the surfactant solution includes a solvent that is a solvent to the surfactant but a non-solvent to the superabsorbent material and the surfactant solution includes an amount of water sufficient to solvate the surface of the superabsorbent material but less than sufficient to cause significant swelling of the superabsorbent material.

The invention further includes permanently wettable superabsorbent materials, such as fibers, made by the method and disposable absorbent products comprising the permanently wettable superabsorbent material. The permanently wettable superabsorbent materials made by the method have a floating time less than 30 seconds and cause a reduction in surface tension of saline less than about 30%.

An object of the invention is to provide superabsorbent fibers, and methods of making same, exhibiting a permanently wettable surface ( $\theta < 90^\circ$  and floating time of less than 30 seconds) and causing a low reduction in surface tension of fluid, desirably less than or equal to about 30% reduction in surface

tension of saline (0.9% NaCl), more desirably less than or equal to about 25%, and more desirably 20%, reduction in surface tension of saline.

### Detailed Description of the Invention

5 Superabsorbent fibers (SAFs) have the potential for better fluid distribution properties than superabsorbent particles (SAPs) due to the smaller dimension and larger surface area of fibers. However, commercially available SAFs, such as Fiberdri® from Camelot Superabsorbents Ltd. of Calgary, Canada and Oasis® from Technical Absorbents UK, are actually worse in fluid  
10 distribution properties than commercially available SAPs. One commonly advanced reason for this poorer performance is the faster fluid pickup rate of superabsorbent fibers. However, there are at least two other causes of this inferiority. First, the surface of a SAF is made hydrophobic during the fiber spinning process. Second, surfactants applied to the fiber to counteract the fiber's hydrophobicity may be released from the fiber into liquid that comes in contact with the fiber, and lower the surface tension of the liquid.

Disclosed herein are permanently wettable (hydrophilic) superabsorbent fibers which do not cause a significant reduction in saline surface tension when placed in saline, and methods to modify superabsorbent fibers into  
20 such materials. The term "permanent" as used herein does not necessarily mean that the superabsorbent remains wettable for an indefinite period of time but rather means that the superabsorbent remains wettable at least upon repeated washings and upon normal usage. Composites containing the permanently wettable superabsorbent fibers exhibit improved fluid distribution  
25 properties over composites containing other SAFs. While the invention is described herein particularly as a method to make permanently wettable superabsorbent fibers, it should be understood that it is also applicable to making other forms of permanently wettable superabsorbent materials such as, for example, a particulate, a film, a nonwoven, a bead, a foam, and a coform.

The belief that superabsorbent fibers should exhibit improved fluid distribution over SAPs is based on the Laplace equation:  $p = 2 \gamma \cos \theta / R_c$  (where  $p$  is capillary pressure,  $\gamma$  is surface tension of fluid,  $\theta$  is the contact angle at the liquid-solid-air interface, and  $R_c$  is the capillary radius). Due to a significant reduction in the capillary radius,  $R_c$ , from SAPs to SAFs, the capillary pressure  $p$  should have a significant increase, which means an increase in fluid distribution power. However, SAFs have actually been found to perform worse than SAPs in fluid distribution in some cases.

Without meaning to be held to theory, it is believed that the reason for the poorer results is that the SAF surface is hydrophobilized during the spinning process. For example, sodium polyacrylate, a commonly used superabsorbent material, is a hydrophilic polymer due to the presence of carboxyl groups ( $-\text{COO}^-$ ) and carboxylic acid groups ( $-\text{COOH}$ ). However, the surface of a sodium polyacrylate fiber can be very hydrophobic if a solution of the polymer is dried in hot air. That is because hot air is hydrophobic relative to water so that hot air attracts more hydrophobic segments  $(-\text{C}-\text{C}-)_n$  of the sodium polyacrylate onto the surface and at the same time repels the hydrophilic segments ( $-\text{COO}^-$ ,  $-\text{COOH}$ ) of the polymer away from the surface. This is so-called surface hydrophobization. Surface hydrophobicity is one of the reasons why SAFs do not exhibit improved fluid distribution properties. A hydrophobic surface is one with a contact angle  $\theta$  greater than  $90^\circ$ , which results in a negative capillary pressure in the Laplace equation.

In order to make wettable superabsorbent fibers, others have applied surfactant onto the fibers to improve their contact angle and wettability. This approach can solve the surface wettability problem but creates another problem. The surfactant applied does not permanently stay on the surface of the superabsorbent fibers due to the surfactant used and the methods of application. The surfactant on the surface of superabsorbent fibers is fugitive and will be dissolved into the fluid contacting the fiber, which dramatically reduces the

surface tension  $\gamma$  of the fluid and negatively hinders fluid distribution properties.

The methods of the invention involve application of a reactive surfactant to the surface of a superabsorbent fiber when the fiber is activated.

5 There are several ways to achieve this. In a desired method particularly described herein, the surfactant is applied to the fiber when the fiber is solvated. The surfactant is applied to the fiber in a liquid that is a solvent for the surfactant but not for the fiber. Water is added to the surfactant solution. The amount of water should be enough to solvate the surface of the fiber so that  
10 ionic groups on the surface macromolecules of the fiber can be freed to rotate to promote interaction with the functional reactive groups of the surfactant. However, the amount of water should not be enough to cause significant swelling of the fiber. The fiber can be treated with the surfactant/water/solvent solution in a number of ways, including spraying or immersion. The treated  
15 fiber can be washed, if desired, and then dried to remove the solvent and water.

Other methods can be used to promote interaction between the functional groups of the surfactant and the SAF. For example, the SAF can be exposed to a higher humidity environment for a while and then treated with the surfactant. The water vapor will solvate the surface of the SAF to achieve  
20 the same solvated state as the liquid water. Another example is that the SAF can be exposed to a high energy radiation, such as e-beam or plasma, and then treated with the surfactant. Such radiation can activate the surface macromolecules, generating free radicals or ions, which promotes reaction with the surfactant.

#### 25 Fibers

Any of a number of superabsorbent fibers can be used in the invention. As used herein, the term "superabsorbent" refers to a water-swella-  
ble, water-insoluble material capable, under the most favorable conditions, of absorbing at least about 10, desirably of about 20, and often of up to  
30 about 1000 times its weight in water. Organic materials suitable for use as a

superabsorbent material of the present invention may include natural materials such as agar, algin, carrageenan, starch, pectin, guar gum, chitosan, and the like, modified natural materials such as carboxyalkyl cellulose, methyl cellulose, hydroxyalkyl cellulose, chitosan salt, dextran, and the like; as well as synthetic materials, such as synthetic hydrogel polymers. Such hydrogel polymers include, but are not limited to, alkali metal salts of polyacrylic acids, polyacrylamides, polyvinyl alcohol, ethylene maleic anhydride copolymers, polyvinyl ethers, hydroxypropylcellulose, polyvinylmorpholinone, and polymers and copolymers of vinyl sulfonic acid, polyacrylates, polyacrylamides, polyvinyl amines, polyallylamines, polyvinylpyrrolidone, and the like. Other suitable polymers include hydrolyzed acrylonitrile grafted starch, acrylic acid grafted starch, and isobutylene maleic anhydride copolymers and mixtures thereof. The hydrogel polymers are desirably lightly crosslinked to render the material substantially water insoluble. Crosslinking may, for example, be by irradiation or by covalent, ionic, van der Waals, or hydrogen bonding.

In one embodiment of the present invention, the absorbent fibers comprise one or more superabsorbent materials in the form of a sodium salt of a cross-linked polymer. Such superabsorbent materials include, but are not limited to, Fiberdri® 1161, Fiberdri® 1231, and Fiberdri® 1241 (all available from Camelot Superabsorbent Ltd. of Calgary, Canada); and Oasis® 101, Oasis® 102, and Oasis® 111 (all available from Technical Absorbents, UK).

The superabsorbent fibers can be made by a number of methods known to those skilled in the art.

#### Surfactants

Suitable surfactants are compounds having at least one functional group reactive with the SAF and at least one non-reactive and hydrophilic functional group. Reactive functional groups include cationic groups for an anionic SAF and anionic groups for a cationic SAF. Examples of cationic groups are, without limitation, quaternary ammonium groups, and amino groups when the anionic SAF contains acidic groups such as carboxylic acid groups. Examples of anionic groups are, without limitation, carboxyl groups, sulfonate

groups, phosphate groups, and their corresponding acid groups when the cationic SAF contains basic groups such as amino groups.

Non-reactive, hydrophilic functional groups include, without limitation, hydroxyl groups, ether groups, carboxylic acid groups, amino groups, and imino groups.

One suitable surfactant is Rhodamox LO (lauryl dimethylamine oxide) from Rhone-Poulenc, Inc. The surfactant solution desirably has a concentration of about 0.001 g to 20 g surfactant per 1000 g solvent, more desirably about 0.005 g to 10 g surfactant per 1000 g solvent, more desirably about 0.01 g to 5 g surfactant per 1000 g solvent, and more desirably about 0.05 to 1 g surfactant per 1000 g solvent.

#### Solvents

The solvent has to be compatible or miscible with the SAFs' activating agent, such as water. The solvent is one which solvates the surfactant but does not substantially solvate the fiber. Appropriate solvents can be selected by those skilled in the art and include, without limitation, isopropanol, methanol, ethanol, butyl alcohol, butanediol, butanetriol, butanone, acetone, ethylene glycol, propylene glycol, glycerol, and mixture of the above. Preferred solvents include isopropanol, ethanol, and acetone.

#### Amount of Water

The amount of water to be added is important; it should be enough to solvate the surface of the fiber so that ionic groups on the surface macromolecules of the fiber can be freed to rotate to promote interaction with the functional groups of the surfactant. However, the amount of water should not be enough to cause significant swelling of the fiber. Significant swelling of a SAF is defined as a volume increase of at least about 100%.

A desired amount of water is from 0.5 to 30 weight % by total weight of the solvent, desirably from about 1 to 20%, more desirably from about 1 to 15%, most desirably from about 1 to 10%. All percentages herein are by weight unless otherwise stated.



While not meaning to be limited to theory, the water is believed to act as an activation agent to promote reaction between the reactive functional groups of the surfactant and the functional groups of the superabsorbent fiber. For example, if a cationic/non ionic surfactant is applied onto the surface of polyacrylate superabsorbent fiber in the absence of water, anionic groups (-COO<sup>-</sup>) of the fiber are not present on the surface due to the surface hydrophobization or are not in the ionic form due to lack of water. Though the surfactant has cationic groups they cannot form ionic bonds with the anionic groups of the fiber. The surfactant just adheres to the surface of the fiber and becomes fugitive. However, when a certain amount of water is present in the treating solution, the water can solvate the surface of the fiber and the anionic groups near the surface of the fiber will be able to rotate from an inward conformation to an outward conformation which allows the cationic groups of the surfactant to form ionic bonds with these outward anionic groups and achieve a permanent surface wettable treatment.

#### Reaction Conditions

The fiber can be treated with the surfactant solution in a number of ways, including spraying or immersion. The ratio of SAF to treating solution will vary greatly depending upon how the surfactant is applied to the fiber. For example, a ratio of 1:1 (grams of SAF to grams of solution) to 1:5 is desirable when the solution is applied by spraying. In one embodiment of immersion treatment, the SAF is added into the pre-prepared treating solution. The ratio of SAF to treating solution will desirably range from about 1:1 to 1:500, more desirably from about 1:1 to 1:100, more desirably from about 1:1 to 1:50.

The treatment is carried out at a temperature from about 0°C to 100°C, more desirably from about 10 to 60°C, more desirably about 20 to 30°C, desirably about room temperature (23°C). The length of treatment depends upon the method of application, the temperature of application, as well as the components. The length of treatment will range from about 0.01 to 1 hour, desirably from about 0.05 to 0.5 hour, more desirably from about 0.1 to 0.3 hour, desirably with constant agitation.

### Washing and Drying

5 The purpose of washing is to remove any fugitive surfactant. Even  
when a reactive surfactant and proper reaction conditions are selected, fugitive  
surfactant can still be generated when too much surfactant is used (number of  
10 surfactant molecules is more than number of available functional groups on the  
surface of the SAF or there is incomplete reaction between the surfactant and  
the functional groups of the SAF). An effective washing applies a weight ratio  
of SAF to washing solvent in a range of about 1:2 to 1:500, desirably about 1:5 to  
1:200, more desirably about 1:10 to 1:100. Washing at room temperature is  
15 preferred, however, a temperature ranging from 0°C to 100°C can be used. A  
mixing aid, such as mechanical agitation, vibration, or ultrasonic treatment, will  
help to achieve a higher effectiveness of the washing. The liquid used for  
washing will be a solvent for the surfactant but not for the fiber.

Any conventional drying method, such as air drying at ambient  
condition or at an elevated temperature, vacuum drying, freeze drying,  
supercritical drying, etc., can be used to dry the treated and/or washed fibers.

20 The superabsorbent fibers of the present invention are suitable for  
use in disposable absorbent products such as personal care products, such as  
diapers, training pants, baby wipes, feminine care products, adult incontinent  
products, and medical products, such as wound dressings, surgical capes, and  
drapes.

25 The SAFs can be used in woven and nonwoven products as  
commercially available superabsorbent fibers are now used. It may be desirable  
to mix the inventive superabsorbent fibers with other fibers and/or to add  
superabsorbent particles to a web made of the inventive fibers to make an  
absorbent structure. The invention disclosed can also be applied to other forms  
of superabsorbents, such as particulates, films, flakes, nonwovens, beads, and  
foams to improve their surface wettability.

30 In one embodiment of the present invention, a disposable  
absorbent product is provided, which includes a liquid-permeable topsheet, a

backsheet attached to the topsheet, and an absorbent structure made with the inventive fibers positioned between the topsheet and the backsheet.

Disposable absorbent products, according to all aspects of the present invention, are generally subjected during use to multiple insults of a body liquid. Accordingly, the disposable absorbent products are desirably capable of absorbing multiple insults of body liquids in quantities to which the absorbent products and structures will be exposed during use. The insults are generally separated from one another by a period of time.

Those skilled in the art will recognize materials suitable for use as the topsheet and backsheet. Exemplary of materials suitable for use as the topsheet are liquid-permeable materials, such as spunbonded polypropylene or polyethylene having a basis weight of from about 15 to about 25 grams per square meter. Exemplary of materials suitable for use as the backsheet are liquid-impervious materials, such as polyolefin films, as well as vapor-pervious materials, such as microporous polyolefin films.

The invention is further illustrated by the following examples, which are not to be construed in any way as imposing limitations upon the scope thereof. On the contrary, it is to be clearly understood that resort may be had to various other embodiments, modifications, and equivalents thereof, which, after reading the description herein, may suggest themselves to those skilled in the art without departing from the spirit of the present invention.

### Examples

Two properties of SAFs were measured in Example 1: floating time, to indicate surface wettability, and surface tension using a saline solution, to indicate fugitiveness of the surfactant. In Example 2, an inclined wicking test was used to evaluate fluid distribution properties of composites including the inventive SAF samples. The Free Swell, dry weight, density, and saline pick-up are also reported. The testing procedures are summarized below:

Floating Time: about 80 g of 0.9% NaCl isotonic saline, available from RICCA Chemical Co. (Arlington, TX), was placed in a 100 ml beaker. 0.01 g

of superabsorbent fiber was weighed and gently added to the beaker from a height about 5 cm above the surface of the saline. The time from when the fiber first contacted the surface of the saline to the time the fiber was below the surface of the saline was recorded as Floating Time.

5                   Surface Tension Test: One gram of superabsorbent fiber was thoroughly mixed with 150 grams of 0.9% NaCl saline in a flask. After 15 minutes, the saline was poured into a glass container. A Kruss Processor Tensiometer K 12 was used to measure the surface tension of the treated saline.

10                   Absorbency Tests: About 0.16 g of superabsorbent fiber was weighed and placed into a plastic AUL test cylinder with a 100 mesh screen on its bottom. A plastic piston was placed on the top of the discs which generated a pressure of about 0.01 psi. The cylinder was then placed into a dish which contained about 50 ml of 0.9% NaCl saline. After 1 hour, the cylinder was taken out and placed on paper towel to blot interstitial fluid. The blotting was continued by moving the cylinder to dry paper towel until there was no fluid mark visible on the paper towel. The weight difference of the cylinder between wet and dry represented total amount of fluid absorbed by the SAF and was reported as the Free Swell Absorbency. The Absorbency Test is described in more detail in WO 99/17695 in the section titled "Flooded Absorbency Under Zero Load".

15 20 25                   Inclined Wicking Test: Superabsorbent fiber samples were air laid with wood pulp fluff into composites having a total basis weight of 400 gsm. The composites were densified to about 0.2 g/cc and cut into a size of 33 cm by 5.1 cm. A cut sample was placed into an inclined wicking trough (inclined angle of 30°) for the wicking test. The testing fluid was 0.9% NaCl saline. The test lasted about 90 minutes and both wicking distance and wicking capacity (pick-up) were recorded as parameters to reflect fluid distribution capabilities. The Wicking Test is described in more detail in European Publication 761 192 A2 in the section titled "Wicking Parameter".

30                   Density was determined by dividing the basis weight by the thickness of the web. The thickness was determined using a Digimatic Indicator

Model 1DF-150E, available from Mitutoyo Corporation, Japan, with an applied pressure of 0.05 psi and an accuracy of 0.001 mm.

Example 1: Formation of Wettable and High Surface Tension Fibers

A commercially available superabsorbent fiber (Fiberdri 1241-  
5 available from Camelot Superabsorbent Ltd. of Calgary, Canada) was used. This  
fiber is a crosslinked copolymer of maleic anhydride and isobutylene. This fiber  
is wettable (floating time less than 30 seconds) but causes a surface tension  
reduction of saline (0.9% NaCl) from 72 to 47 dyne/cm (34.7% reduction). The  
fiber was washed up to six times in isopropanol (weight ratio of fiber to  
10 isopropanol about 1 to 10) to remove any surfactant that came with the  
superabsorbent fiber. Each washing time was about 1 hour. Fresh isopropanol  
was added to the fiber for each washing. The results in Table 1 for samples 1-7  
show that floating time of the fiber and surface tension of the saline increased  
with each washing, indicating that surfactant was indeed washed off of the fiber  
15 and that the surface of the fiber became more hydrophobic.

In a second step, the washed SAF was treated with a  
cationic-nonionic surfactant, Rhodamox LO (lauryl dimethylamine oxide),  
available from RhonePoulenc, Inc., in an isopropanol medium with (Sample 9)  
or without (Sample 8) water. The weight ratio of  
20 SAF/water/isopropanol/Rhodamox LO was 1:1:50:0.005. The treated fiber was  
then washed with fresh isopropanol to ensure that no unreacted surfactant was  
left on the surface of the fiber. The results of the floating test and surface tension  
tests show that the fiber treated in the presence of water was permanently  
wetable, with a floating time of 26.1 seconds, and maintained a surface tension  
25 of 57.5 dyne/cm (20% reduction).

Table 1

Sample No.	Superabsorbent Fibers	Floating Test (seconds)	Surface Tension (dyne/cm)
1	Fiberdri 1241 as received	19.1	47.8
2	Fiberdri 1241 washed once	59.5	54.2
3	Fiberdri 1241 washed twice	greater than 60	--
4	Fiberdri 1241 washed 3x	greater than 60	--
5	Fiberdri 1241 washed 4x	greater than 60	56.9
6	Fiberdri 1241 washed 5x	greater than 60	57.1
7	Fiberdri washed 6x	greater than 60	58.1
8	Fiberdri 1241 washed 6x and treated with cationic surfactant (without water)	24.6	44.3
9	Fiberdri 1241 washed 6x and treated with cationic surfactant (with water)	26.1	57.5

Example 2: Formation and Testing of Composites

Sample Nos. 1, 7, and 9 from Example 1 were used as fiber samples in Example 2. Sample No. 1 was selected to represent a wettable but low surface tension fiber, sample No. 7 was selected to represent a non-wettable but high surface tension fiber, and sample No. 9 was selected to represent a wettable and high surface tension sample. Each fiber sample was made into a composite through an air forming process.

The composites were made using an air former. The air former consists of two compartments. The first compartment is a cylindrical chamber having a diameter of about 2 feet and a height of about 1 foot and equipped with 10 air nozzles connecting with a source of compressed air. This chamber is for the purpose of mixing components intended to add into the composite. The

compressed air will generate a strong turbulence to aid mixing. The second chamber, called the air laying chamber, has a dimension of about 1.5' (L) x 0.5' (W) x 2.5' (H) and is connected with a vacuum source. The SAF and wood pulp fluff were added into the first chamber at a certain ratio, mixed by the air turbulence and then sucked into the second chamber under vacuum through a metal screen which connects the two chambers. Fully homogenized components were air laid on a sheet of forming tissue to form the composite. The composite prepared was compressed by a Carver press at a temperature of 150°C and a pressure of 500 psi for 10 seconds.

Each composite included 60% superabsorbent fiber and 40% wood pulp fluff fiber (Coosa CR1654 produced by US Alliance Coosa Pines Corporation, Alabama), and had a basis weight of 400 grams per square meter (gsm). The composites were densified to around 0.2 g/cc using a Carver press. The composites were cut into 2" (5.08 cm) by 13" (33.02 cm) stripes and a stripe was placed into a trough having an inclined angle of 30° to the horizontal to measure inclined wicking distance and wicking capacity. Table 2 below summarizes the results.

Table 2

Composite No.	SAF No.	Free Swell of SAF (g/g)	Dry Weight (g)	Density (g/cc)	Saline Pick-Up (g)	Wicking Distance (cm)
1	1	30.0	6.66	0.184	64.6	15.2
2	7	30.7	6.40	0.177	68.5	15.2
3	9	29.4	6.75	0.188	86.6	18.2

Note the greater wicking distance and higher wicking capacity for the inventive SAF containing composite.

The above description is intended to be illustrative and not restrictive. Many embodiments will be apparent to those of skill in the art upon reading the above description. The scope of the invention should, therefore, be

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